

HYBRID LENS WITH HIGH NUMERICAL APERTURE

BACKGROUND OF THE INVENTION

5 This application claims priority from Korean Patent Application No. 2002-69593, filed on November 11, 2002, in the Korean Intellectual Property Office, the disclosure of which is incorporated herein in its entirety by reference.

1. Field of the Invention

10 The present invention relates to a hybrid lens combining a diffractive lens with a refractive lens, and more particularly to a hybrid lens with a high numerical aperture used in an optical information recording/reproducing apparatus.

2. Description of the Related Art

15 The development of an optical information media has led from CDs (Compact disks) having a diameter of 12 cm and a substrate thickness of 1.1 mm to DVDs (Digital Versatile Disks) having a diameter of 12 cm and a substrate thickness of 0.6 mm and is further leading toward blue-ray disc that are thinner than DVDs. Optical apparatuses for recoding and reproducing information from such optical information media have also been researched and developed so that high recording density can be achieved by focusing high optical energy into a small spot. For example, an optical recoding/reproducing apparatus for CDs adopts a light source having a wavelength of 780nm and a lens having a numerical aperture (NA) of 0.45. Meanwhile, an optical recoding/reproducing apparatus for DVDs adopts a light source having a wavelength of 680nm and a lens having a numerical aperture of 0.6. The blue-ray disc which is still being researched actively is designed for a light source having a wavelength of about 405nm and a lens having a numerical aperture of about 0.85. However, manufacturing a lens with such a high numerical aperture is still difficult with a current technology.

25 FIG. 1 is a diagram showing the relationship between numerical aperture (NA), spot size and depth of focus Δz of a general lens 11.

30 In FIG. 1, D denotes an aperture of the lens 11, f denotes a focal length and θ denotes an angle of refraction of the light transmitted through the lens. The following Equation 1 defines numerical aperture (NA), wherein n denotes a refractive

index of the lens and θ denotes a refractive angel thereof. The following Equation 2 gives the relationship between spot size ω_0 , numerical aperture NA and wavelength λ , when an incident beam is parallel. The following Equation 3 gives the relationship between depth of focus Δz , numerical aperture NA and wavelength λ .

$$NA = n \sin \theta \quad \dots \quad (1)$$

$$\omega_0 = \frac{2}{\pi} \frac{\lambda}{NA} \quad \dots \quad (2)$$

$$\Delta z = \frac{\lambda}{2NA^2} \quad \dots \quad (3)$$

Spot size should be reduced in order to increase information recording density, and according to Equation 2, wavelength λ should be reduced and numerical aperture NA should be increased in order to reduce spot size ω_0 . Accordingly, to record and reproduce information on a blue-ray disc, a blue laser with a short wavelength and a lens with a high numerical aperture are required.

However, it is necessary to increase the depth of focus Δz for a stable recording and reproduction, and according to Equation 3, it is necessary to increase the wavelength λ and decrease the numerical aperture (NA) to increase the depth of focus Δz .

To satisfy the Equation 2 and 3, in the case of the blue-ray disc, a cover layer of the disc preferably is manufactured to have about 0.1mm thickness effectively, which prevents the depth of focus from being shortened, which results from the increase of numerical aperture and decrease of wavelength, thereby increasing the information recording density. However, there is a problem in that increasing the numerical aperture occurs reduction of a tilt allowance range (that is, tilt margin) of the recording surface and light axis. The tilt allowance range can be expanded upto a current DVD level by forming a thinner cover layer of about 0.1mm. It is possible to maintain allowable ranges of disc deflection and tilt of the blue-ray disc, as well as apparatus assembly errors, etc. at the same level as in DVDs.

The refractive lens used in the optical recording/reproducing medium changes the wavelength of incident laser depending on temperatures. While the lights with different wavelengths are passed through the refractive lens, they are focused having different focal lengths in the light axis direction. This is called chromatic aberration.

In the prior art, a thick lens with a large radius of curvature, a low refractive index, and a high Abbe number has been proposed in order to achieve a high numerical aperture while reducing chromatic aberration and dispersion. However, such a lens is difficult to manufacture, and it is large and heavy, making it inappropriate for use in a small and lightweight information recording/reproducing apparatus.

SUMMARY OF THE INVENTION

The present invention provides a small and lightweight hybrid lens with a high numerical aperture, having no chromatic aberration.

According to an aspect of the present invention, there is provided a hybrid lens comprising a refractive surface that refracts incident light and a diffractive surface that diffracts light exiting the lens, the diffracting surface designed by a sag satisfying the following Equation:

$$sag = \frac{f_D + m\lambda - \sqrt{f_D^2 + r^2}}{n-1} \quad \dots (4)$$

wherein f_D is a distance from a center peak to a focal point of the lens, r is a height from a center axis to each peak of the lens, n is a refractive index of the lens, λ is the wavelength of incident light, and m is an integer.

The refractive surface has a low-order aspheric profile z satisfying the following Equation 5,

$$z(r) = \frac{cr^2}{1 + \sqrt{1 - (1+k)c^2r^2}} + Ar^4 + Br^6 + Cr^8 + Dr^{10} \quad \dots (5)$$

, wherein c is a curvature of the refractive surface, k is a conic coefficient representing a shape of the refractive surface and A , B , C and D are fourth, sixth, eighth and tenth aspheric coefficients, respectively. Wherein a minimum diffraction pitch of the diffractive surface is preferably $3\mu\text{m}$, the numerical aperture of the refractive surface is preferably above 0.85 and the diffractive surface has a depth L_m satisfying the following Equation 6.

$$L_m = \frac{\lambda}{n-1} \quad \dots (6)$$

According to another aspect of the present invention, there is provided a small and lightweight hybrid lens with a high numerical aperture, capable of removing chromatic aberration by including a low-order refractive surface and a diffractive

surface designed by the profile defined simply in Equation 4.

BRIEF DESCRIPTION OF THE DRAWINGS

The above and other features and advantages of the present invention will
5 become more apparent by describing in detail exemplary embodiments thereof with
reference to the attached drawings in which:

FIG. 1 is a diagram showing the relationship between numerical aperture (NA),
spot size ω_0 and depth of focus Δz of a general lens;

FIG. 2 is a sectional view showing the structure of a hybrid lens according to a
10 preferred embodiment of the present invention;

FIGS. 3A to 3C are views showing chromatic aberration in a refractive device,
a diffractive device and a hybrid device, respectively;

FIG. 4 is a view showing a diffractive surface structure and profile of the
hybrid lens according to the preferred embodiment of the present invention; and

15 FIG. 5 shows results of a simulation of the hybrid lens according to the
preferred embodiment of the present invention.

DETAILED DESCRIPTION OF THE INVENTION

Hereinafter, a hybrid lens according a preferred embodiment of the present
20 invention will be described in detail with reference to appended drawings.

FIG. 2 is a sectional view schematically showing the structure of the hybrid
lens according to the preferred embodiment of the present invention.

With reference to FIG. 2, a hybrid lens 31 according to the preferred
embodiment of the present invention includes a refractive surface 31a formed with a
25 low-order aspheric profile z defined in Equation 5 and a diffractive surface 31b
having a profile sag defined in Equation 4. A process for obtaining Equation 4 will
be described in detail with reference to FIG. 4. Equation 5 is a formula obtained by
selecting only terms below a tenth order from a general formula relating to the
refractive surface, such as the following Equation 7, wherein, k is a conic coefficient,
30 and when k is a value between -1 and 0, the refractive surface is an ellipsoid.

$$z(r) = \frac{cr^2}{1 + \sqrt{1 - (1+k)c^2r^2}} + Ar^4 + Br^6 + Cr^8 + Dr^{10} + Er^{12} + Fr^{14} + \dots \quad (7)$$

For example, in the case that LASFN30, manufactured by SCHOTT Corp.,
having a mid-range refractive index, is used as a material for forming the hybrid lens,

the lens has a refractive index of about 1.83 and a medium amount of dispersion occurs at a wavelength of 408nm. Here, the refractive index or dispersion of the lens material depends on wavelength, and therefore a suitable material should be selected on the basis of the wavelength of the light source.

5 A principle of correcting chromatic aberration in the hybrid lens according to the preferred embodiment of the present invention will be described with reference to FIGs. 3A to 3C.

FIGs. 3A to 3C show chromatic aberration in a refractive device, a diffractive device, and a hybrid device combining the diffractive device with the refractive device, respectively.

10 With reference to FIG. 3a, because the angle of refraction increases as the wavelength decrease, blue (B), green (G) and red (R) light refracted by a refractive device 22 is focused at a progressively greater distance from the refractive device 22. This phenomenon of chromatic aberration, the focal length increasing with wavelength increasing is called.

15 On the other hand, referring to FIG. 3b, because the angle of diffraction increase as the wavelength increases, red (R), green (G) and blue (B) light diffracted by the diffractive device 24 is focused at a progressively greater distance from a diffractive device 24. That is, the diffractive device 24 generates chromatic aberration in which the focal length increases as the wavelength decreases, opposite to the chromatic aberration of the refractive device. Here, the diffractive device 24 is a fault-type in which a phase-type diffractive lattice is formed on one surface of a glass lens. The property of the diffractive device 24, diffracting incident light at an angle that increases, opposite to the refractive device, is an important property.

20 Accordingly, to remove the opposite types of chromatic aberration generated the refractive device 22 and diffractive device 24, a hybrid device 26 combining the two optical devices is constructed as shown in FIG. 3C.

25 In a conventional optical system, a convex lens and concave lens are arranged together in order to correct chromatic aberration, and a suitable shape or material is selected to increase the refractive index of the convex lens in order to assist dispersion of light in the concave lens. However, which these methods are used in an optical system with a large refractive index, there is a disadvantage that aberration such as spherical aberration, chromatic aberration, etc., is increased. However, it is possible to decrease the refractive index of the optical device and

reduce chromatic aberration without increasing another type of aberration by using the-fault type diffractive device.

Because the refractive device of the prior art used so far has a high Abbe number, it is necessary to significantly increase power of the optical device in order to correct chromatic aberration. However, because chromatic aberration in an optical device having a low Abbe number may change significantly even when the power of the optical device is changed only slightly, it is possible to remove spherical aberration or coma aberration, etc., by adopting an optical device with a low Abbe number without increasing the power of the optical device.

The diffractive device, when converted to a general optical device, has a absolute value of the Abbe number of 3.45 as an index representing refractive index to light wavelength. This value is a smaller value by one decimal figure than that of the general optical glass. In the case of designing the optical system, the diffractive device with the low Abbe number has the advantage to correct not only chromatic aberration but also various other types of aberration. The pitch of the diffractive device may be controlled to decrease spherical aberration, as in the aspheric lens.

Accordingly, the hybrid lens according to the preferred embodiment of the present invention can remove chromatic aberration by combining the refractive device having a high Abbe number with the diffractive device having a low Abbe number, and simultaneously remove other types of aberration by appropriately controlling the pitch of the diffractive device.

FIG. 4 is a view showing a diffractive surface structure and profile sag of the hybrid lens according to the preferred embodiment of the present invention.

With reference to FIG. 4, when an optical path difference between an optical path from a point O to a point F and an optical path from a point C to a point F is an integer number of wavelengths, constructive interference occurs and the intensity of a focal point F on a writing surface is maximum. The optical path between the points C and F is the sum of the optical paths between the points C and A ($=\text{sag} \cdot n$), between the points A and D ($=(L_m - \text{sag}) \cdot 1$) and between the points D and F ($=\sqrt{r^2 + f_D^2} \cdot 1$). The optical path between the points O and F is the sum of the optical paths between the points O and B ($=L_m \cdot n$) and between the points B and F ($=F_D \cdot 1$). Accordingly, a condition for constructive interference is given by the following Equation 8.

$$\sqrt{r^2 + f_D^2} \cdot 1 + sag \cdot n + (L_m - sag) \cdot 1 - f_D \cdot 1 - L_m \cdot n = m' \lambda \quad \dots (8)$$

The depth L_m of the diffractive surface of the hybrid lens in Equation 8 satisfies the above Equation 6 and thus a formula defining the diffractive surface of the hybrid lens according to the preferred embodiment of the present invention is obtained by combining Equations 6 and 8 and rearranging the resultant equation for sag, as seen in the following Equation 9.

$$sag = \frac{f_D + (m'+1)\lambda - \sqrt{f_D^2 + r^2}}{n-1} = \frac{f_D + m\lambda - \sqrt{f_D^2 + r^2}}{n-1} \quad \dots (9)$$

Here, m' is an arbitrary integer. Thus, m is used instead of $m'+1$.

FIG. 5 shows results of a simulation of the hybrid lens according to the preferred embodiment of the present invention. In the simulation, a minimum pitch is set to $2.943 \mu m$ and a lens etching depth is processed to $220 \mu m$. Under these conditions, it is found that a wavefront error is $0.0053 \mu m$ smaller than 0.07λ rms (root mean square), a diffraction efficiency is 92.11%, a lens decenter tolerance is $22 \mu m$ smaller than 0.07λ rms, a surface decenter tolerance is $12 \mu m$, a surface tilt tolerance is 0.55 deg smaller than the standard 0.75 deg , and a defocus is 36 nm for a 1 nm wavelength change, smaller than the standard of 80 nm for a 1 nm λ change. Therefore, it is possible to design a hybrid lens having excellent performance in all respects.

The hybrid lens according to the preferred embodiment of the present invention has the advantages of a high numerical aperture above 0.85, no chromatic aberration, has a small tolerance, compact size, lightweight, and it is easy to manufacture.

While the present invention has been particularly shown and described with reference to a preferred embodiment thereof, it will be understood by those of ordinary skill in the art that various changes in form and details may be made therein without departing from the spirit and scope of the present invention as defined by the following claims. For example, the above-mentioned pitch may be adjusted.